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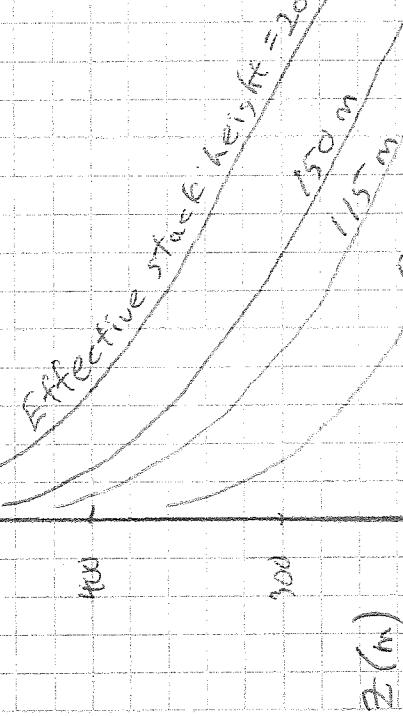
Scan Set A

ATSC 595D
Stuff

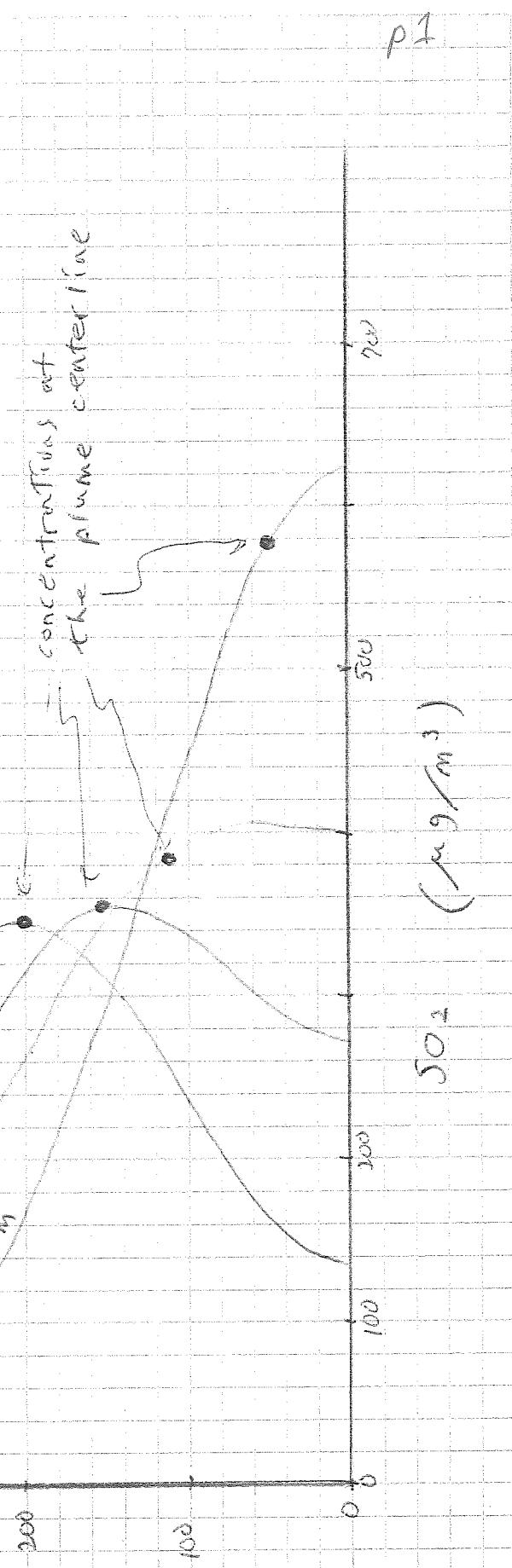
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Example of Reflection from ground (Gaussian Plume)

Vertical concentration profiles from downward plume. Stage 1 by B.



concentrations at
the plume center line



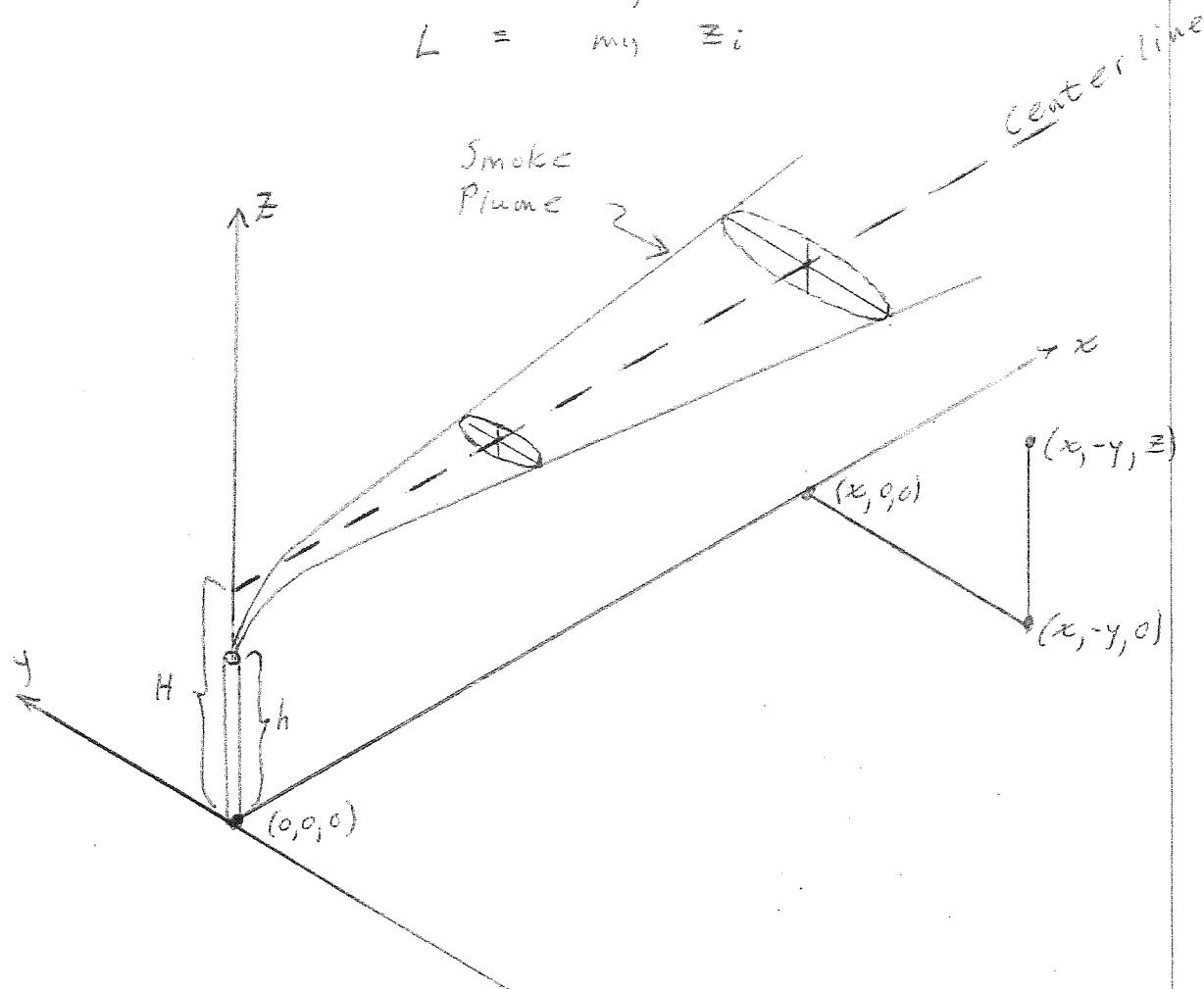
p1

4. Practical Applications of Gaussian Diffusion

a. General Form

(Note: Turner's $\chi = \text{my } C$)

$$L = \text{my } z_i$$



$$C(x, y, z, H) = \frac{Q}{2\pi \sigma_y \sigma_z u} \cdot e^{-\frac{1}{2} \left(\frac{y}{\sigma_y} \right)^2} \cdot \left[e^{-\frac{1}{2} \left(\frac{z-H}{\sigma_z} \right)^2} + e^{-\frac{1}{2} \left(\frac{z+H}{\sigma_z} \right)^2} \right]$$

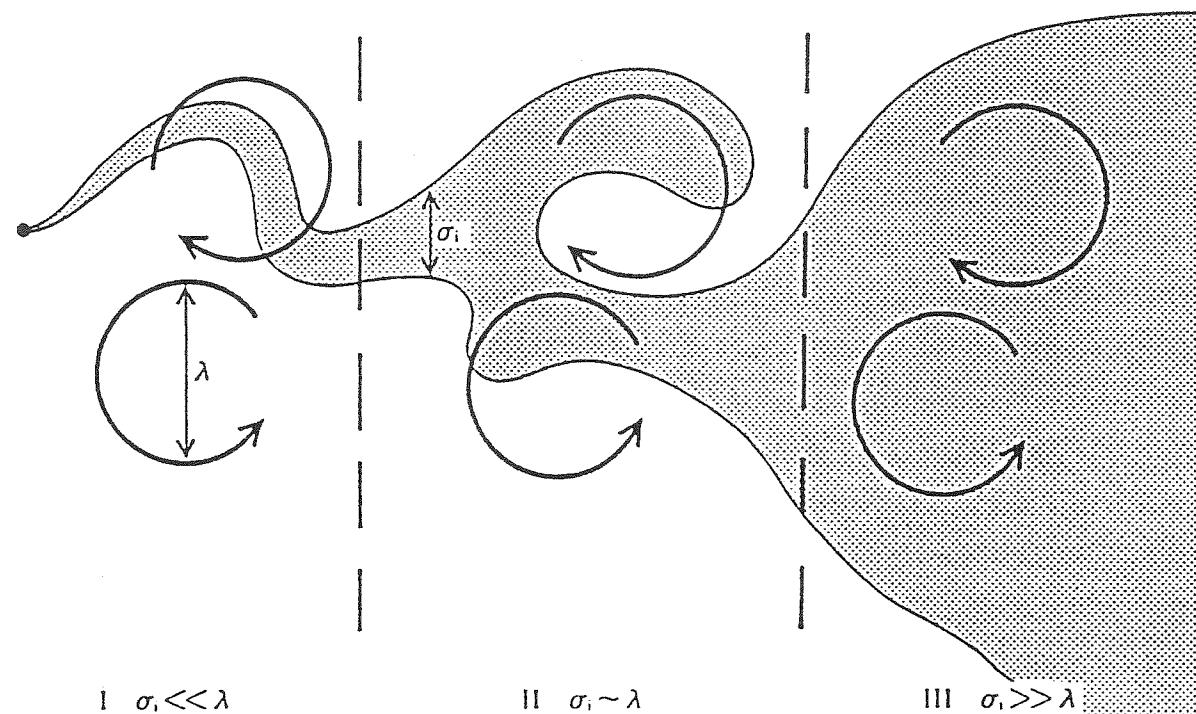
IV.B.4.1

Get σ_y & σ_z from tables, graphs, or
formulas

$$\sigma = \sigma(x, TKE, z_0)$$

See Pasquill & Gifford's curves Turner's Fig 3-2, 3-3
empirical

(a)



(b)

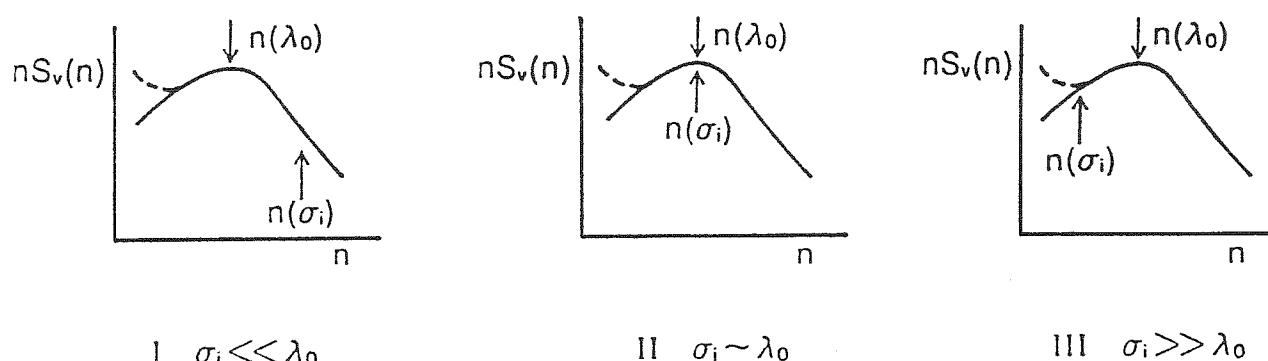
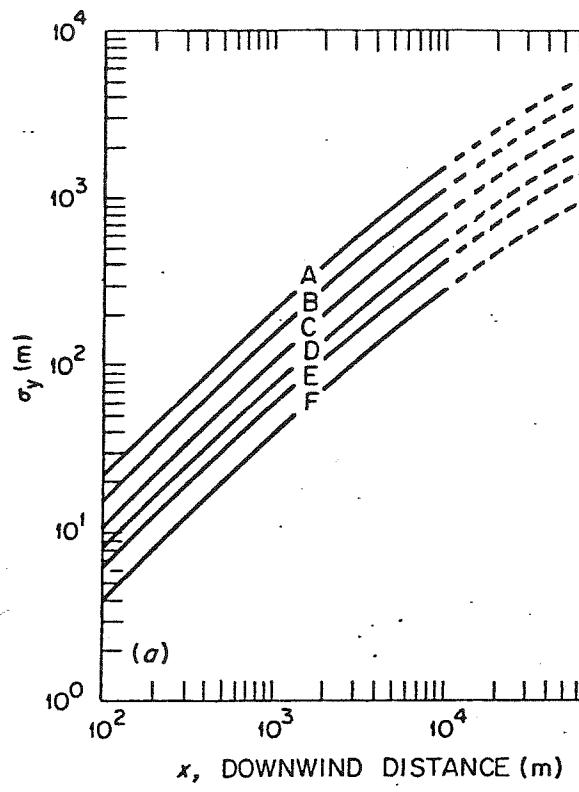


Fig. 9. An illustration of the conceptual model of plume dispersion. Part (a) shows the three different effects of eddies of length scale λ according to the relative size of the crosswind length scale of the instantaneous plume σ_i . Part (b) illustrates how the plume development depends on the form of the velocity spectra, using the example of the horizontal crosswind velocity v . Three regimes are defined similar to those defined in part (a) for the particular length scale λ_0 , corresponding to the peak of the velocity spectrum $S_v(n)$, and the growth and structure of the plume as a whole depends on the relative scales of σ_i and λ_0 as described in the text. The dashed lines show a possible form of the increased energy at low-frequency in stable conditions due to large-scale two-dimensional meandering motions.

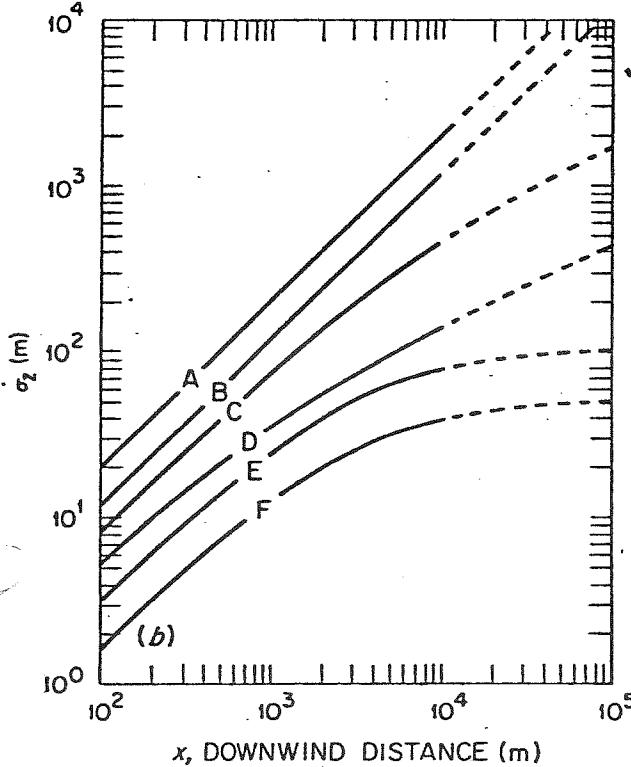
eddies with increasingly large λ , so that this model was able to explain the observation in M&M91 that the inertial subrange extends to lower frequencies at longer range. In stable conditions the observations appear to show that the instantaneous plume is less fragmented at a range of around 100 m than it is in near-neutral stability. This suggests that the process shown in Figure 9aII is reduced and therefore that eddies with $\lambda \sim \sigma_i$ are relatively weak. In order to extend the

Formulas recommended by Briggs (1973) for $\sigma_y(x)$, m, and $\sigma_z(x)$, m; $10^2 < x < 10^4$ m, open country conditions.

Pasquill Type	$\sigma_y(m) =$	$\sigma_z(m) =$
A	.22x(1+.0001x) ^{-1/2}	.20x
B	.16x(1+.0001x) ^{-1/2}	.12x
C	.11x(1+.0001x) ^{-1/2}	.08x(1+.0002x) ^{-1/2}
D	.08x(1+.0001x) ^{-1/2}	.06x(1+.0015x) ^{-1/2}
E	.06x(1+.0001x) ^{-1/2}	.03x(1+.0003x) ⁻¹
F	.04x(1+.0001x) ^{-1/2}	.016x(1+.0003x) ⁻¹



(a)

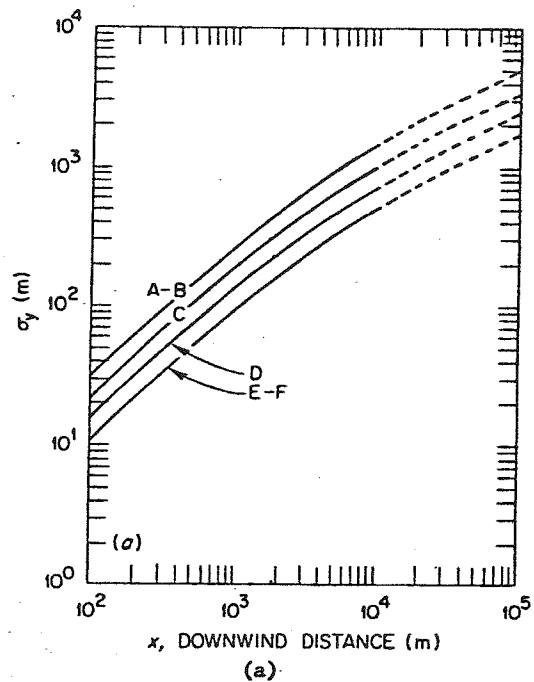


(b)

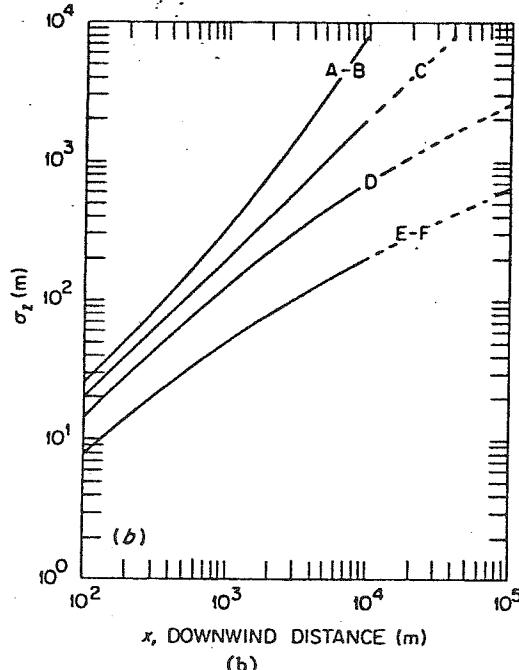
σ_y & σ_z Formulae p4

Formulas recommended by Briggs (1973) for $\sigma_y(x)$, m and $\sigma_z(x)$, m; $10^2 < x < 10^4$ m, urban conditions.

Pasquill Type	$\sigma_y(m) =$	$\sigma_z(m) =$
A-B	.32x(1+.0004x) ^{-1/2}	.24x(1+.001x) ^{1/2}
C	.22x(1+.0004x) ^{-1/2}	.20x
D	.16x(1+.0004x) ^{-1/2}	.14x(1+.0003x) ^{-1/2}
E-F	.11x(1+.0004x) ^{-1/2}	.08x(1+.0015x) ^{-1/2}



(a)



(b)

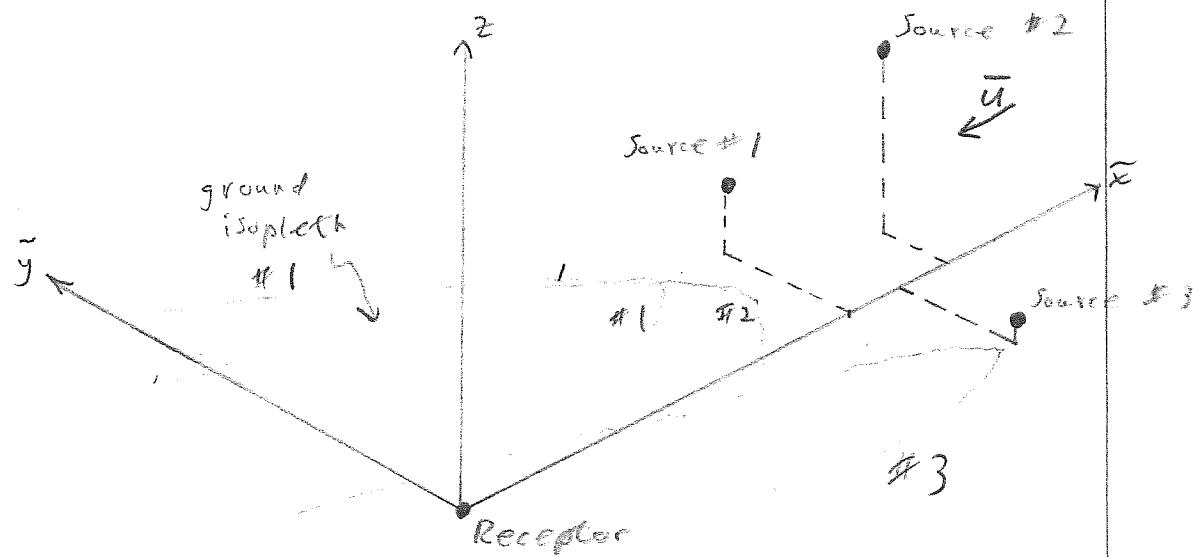
Figure 6. Curves (a) of σ_y and (b) of σ_z based on Briggs' (1973) interpolation formulas for flow over urban areas, see Table 2; from Hosker (1974).

Multiple sources

Superposition

$$C_{\text{Receptor}} = C_1 + C_2 + C_3 + \dots$$

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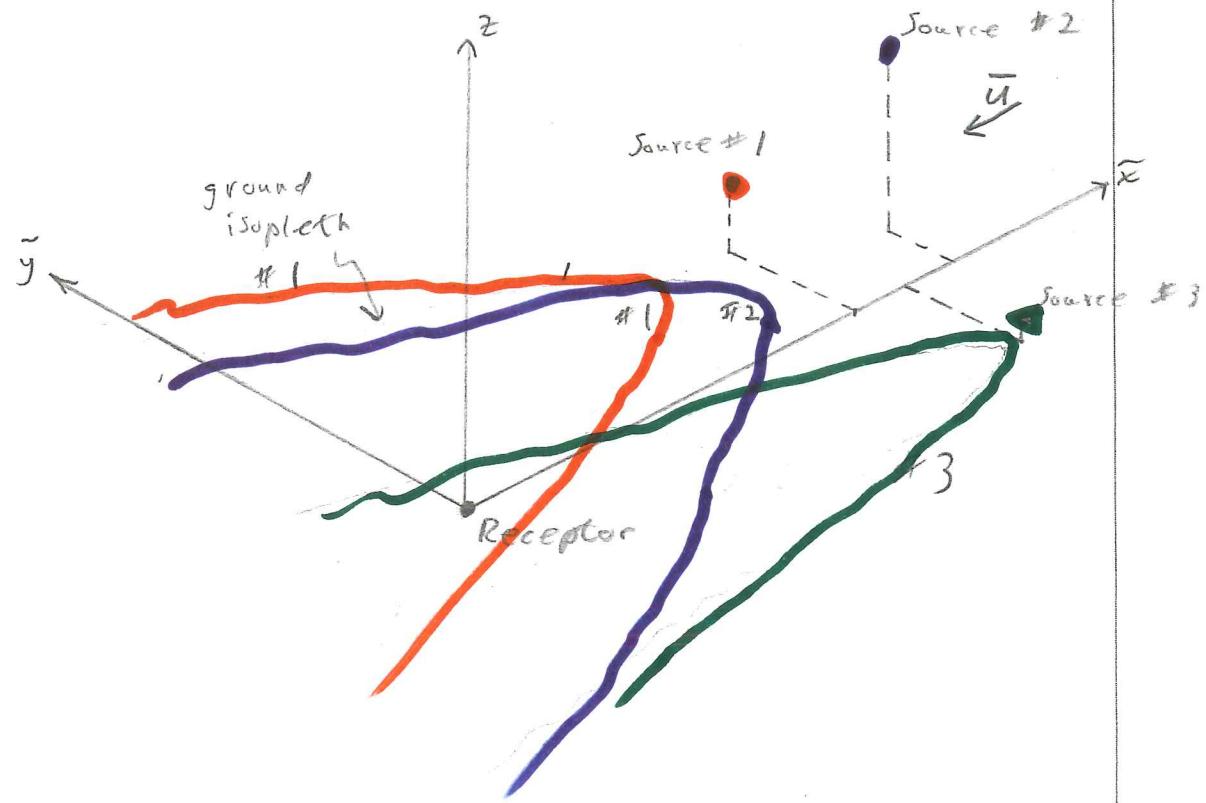
Note, if we are concerned about predicting the point on the ground where the maximum concen will occur, often the easiest way is to manually superimpose plots of ground isopleths & sum.

Multiple sources

Superposition

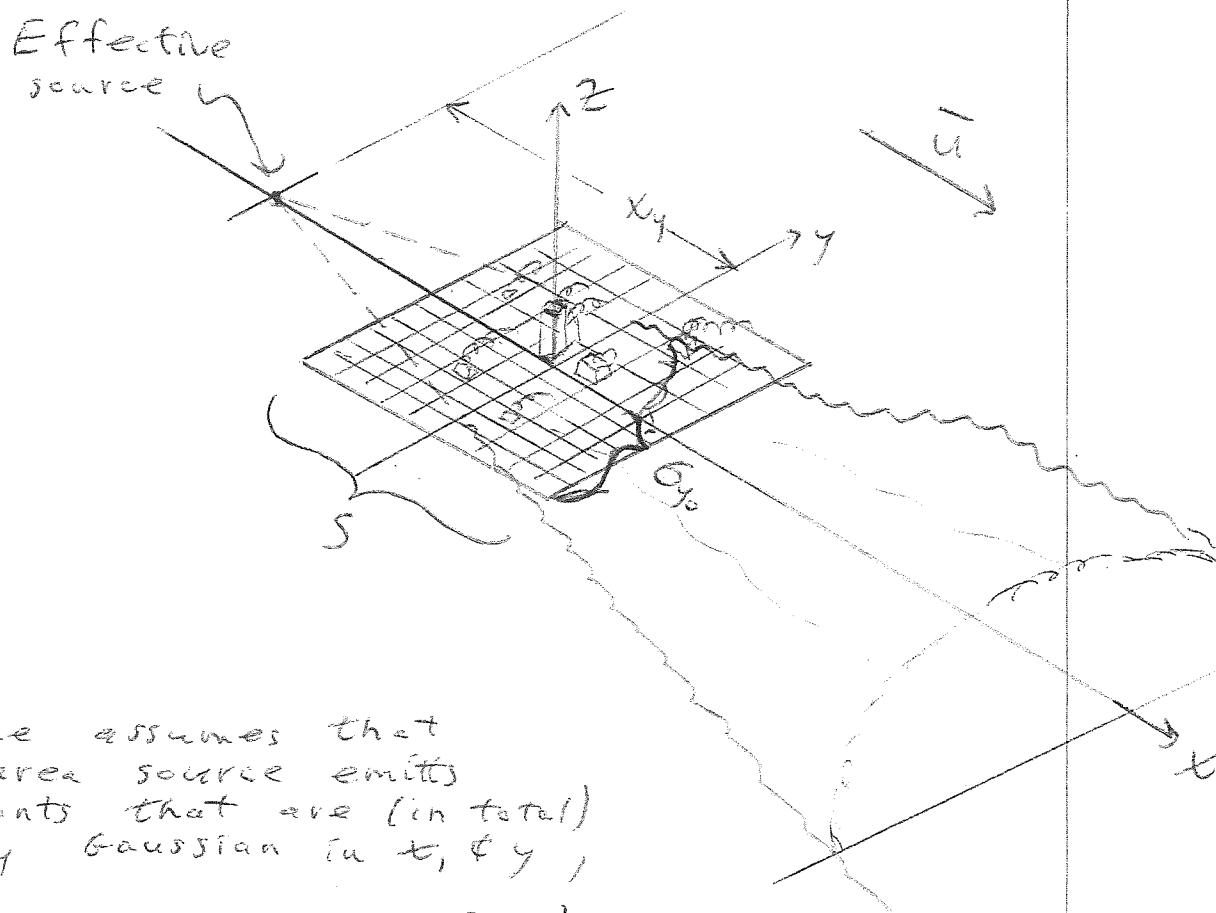
$$C_{\text{Receptor}} = C_1 + C_2 + C_3 + \dots$$

IV.B.4.b



Note, if we are concerned about predicting the point on the ground where the maximum concen will occur, often the easiest way is to manually superimpose plots of ground isopleths, & sum.

c) Point Source approximation to
Area Sources



If one assumes that the area source emits pollutants that are (in total) roughly Gaussian in x , y ,

then we can approximate this by an upwind point source at ground level

Ex/ step 1) Guess σ_y at the area source.

(For a square source, $\sigma_y \approx \frac{s}{4.3}$)
(s = side of square)

2)

Based on the actual stability, go to Fig. 3-2 to find the value of x_0 which would have given the $\sigma_y = \sigma_y$ at the city.

3) Use this ~~approx~~ upwind effective source in the normal point source eqs. to solve for C downwind from point.

Use emission inventory.

Note, if not a ground source, then must solve for x_0 , which may be different from x_0 .