

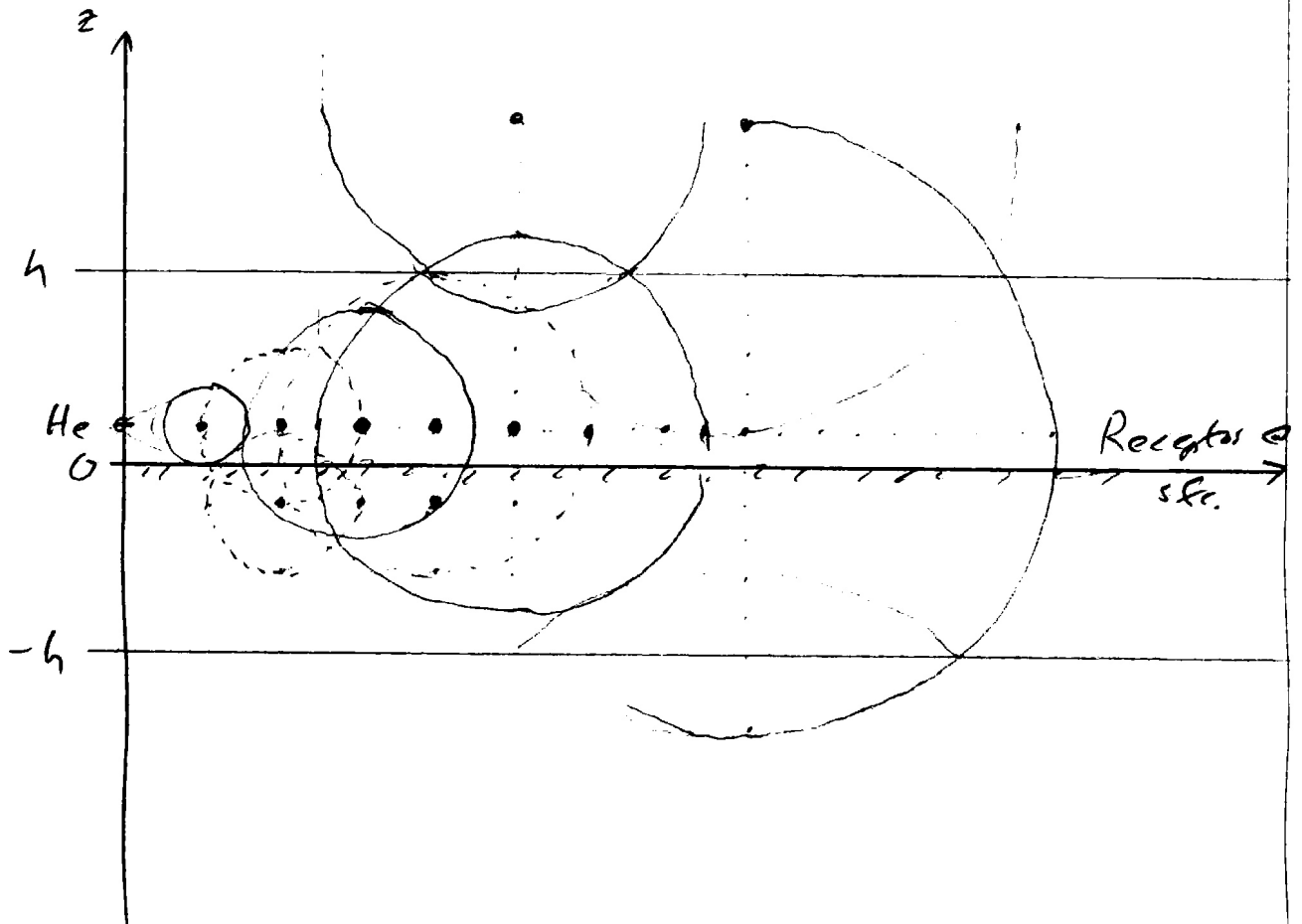
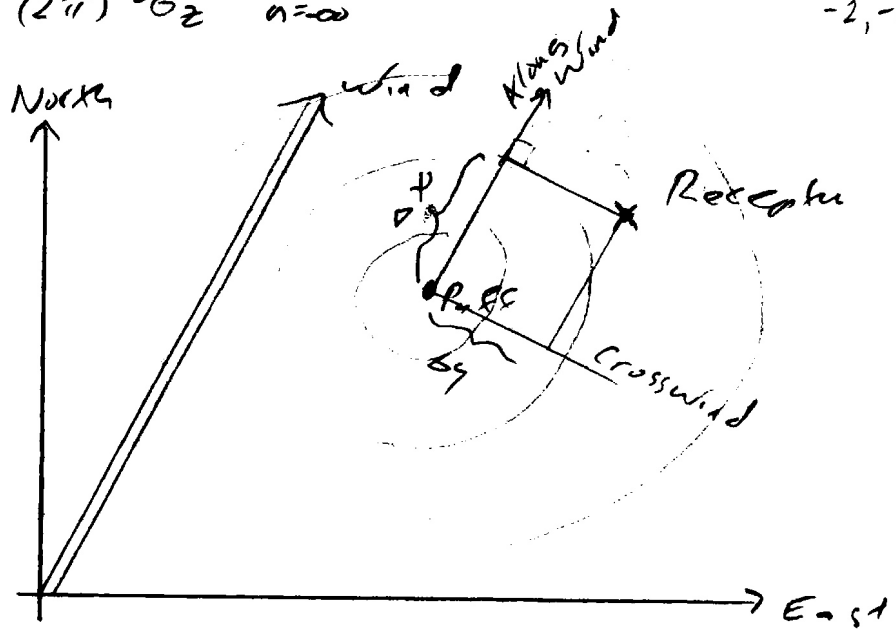
2.1.1 Integrated Puff Sampling Fraction. p 2-4 of Tech Guide

Instantaneous:

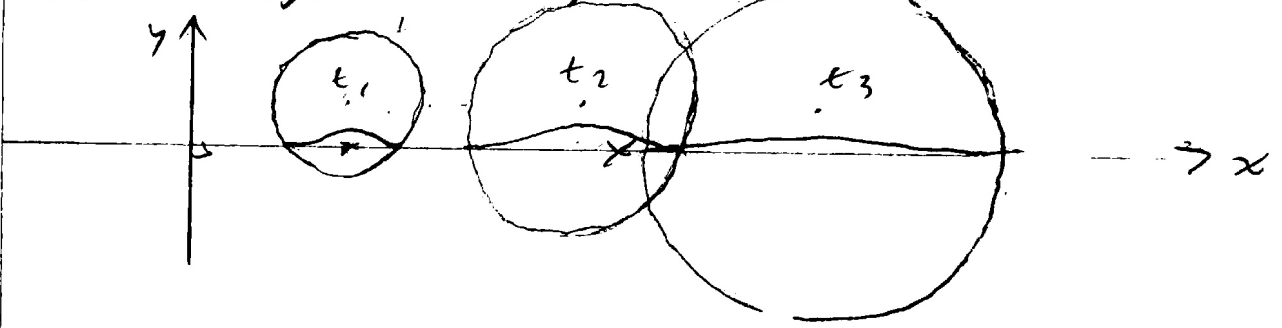
$$C = \frac{Q}{2\pi \sigma_x \sigma_y} g e^{-\frac{1}{2}\left(\frac{dx}{\sigma_x}\right)^2} e^{-\frac{1}{2}\left(\frac{dy}{\sigma_y}\right)^2} \quad \text{Eq (2-1)}$$

where  $g = \frac{2}{(2\pi)^{3/2} \sigma_z} \sum_{n=-\infty}^{\infty} e^{-\frac{1}{2}\left(\frac{H_e + 2nh}{\sigma_z}\right)^2}$  Eq (2-2)  
for n = integer  
-2, -1, 0, 1, 2

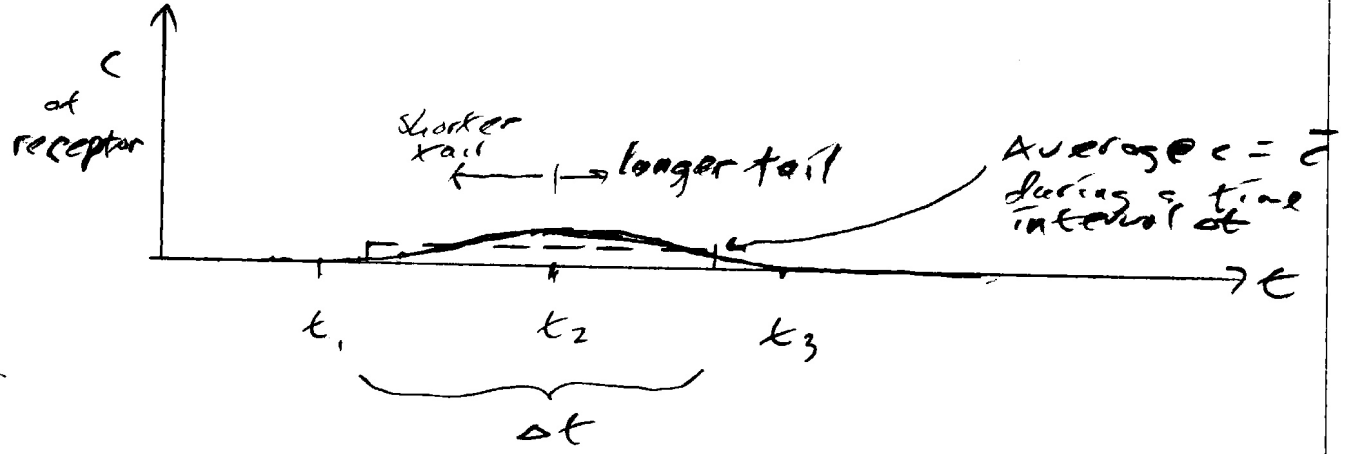
DRAWN



Time Averaged as one puff blow

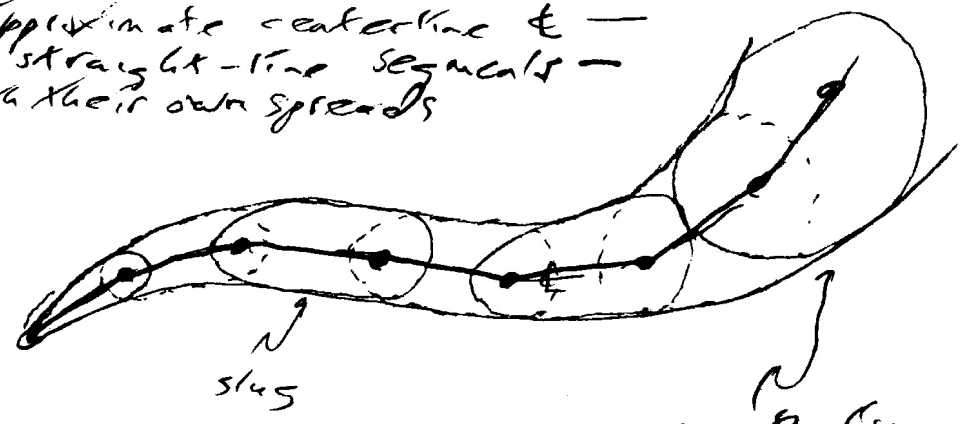


AVRAD



NSITs

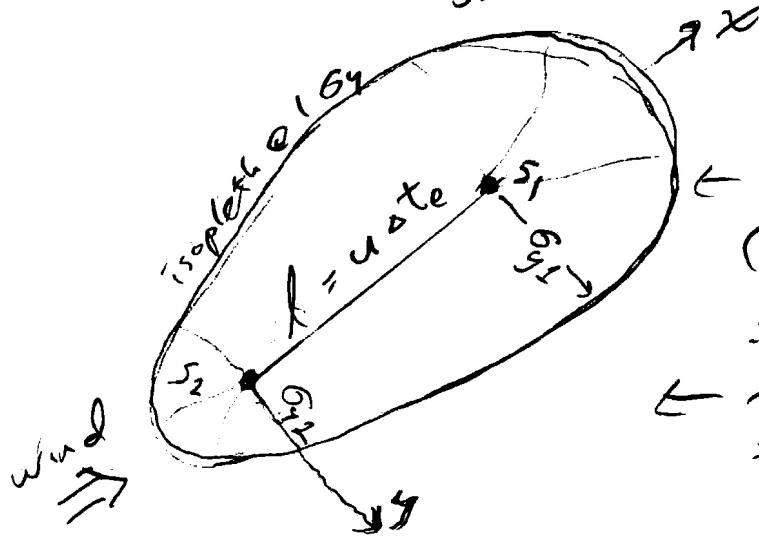
Approximate centerline & —  
by straight-line segments —  
with their own spreads



eventually approach same solution as = large path

AWRAD

- Advantages:- avoids need for excessively large number of paths for initial pump.
- ∴ faster computation. (need to Lagrangian advect only the 2 slug end points). But since each point is shared w 2 slugs,
  - ∴ need only 1 Lagrangian prediction / slug.



← leading point  
(first out of the source)  
∴ oldest

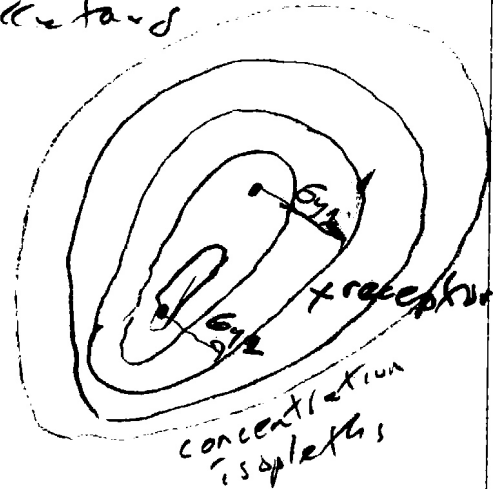
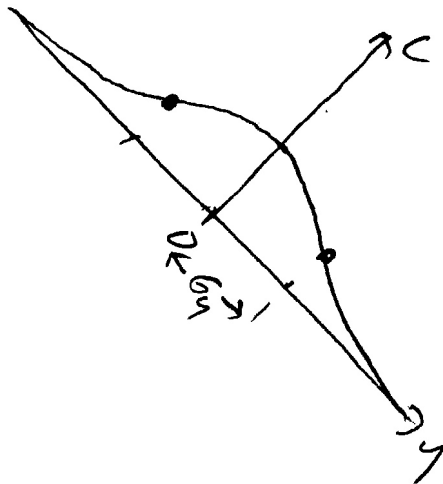
← trailing point  
= youngest

Let:

$u$  = mean wind speed (m/s)

$t_e$  = emission duration for this slug (s)

$\sigma_y$  = cross-wind spread of pollutants



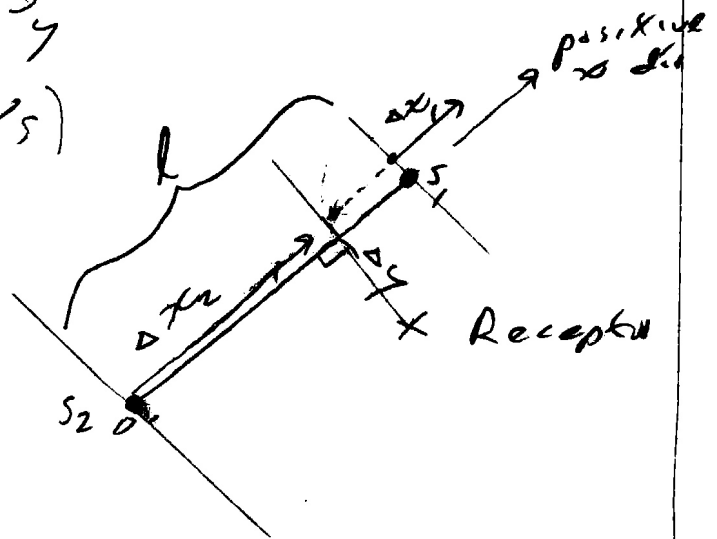
$q$  = emission rate (g/s)

$\Delta x_2$  = distance to receptor from  $S_2$  in direction toward  $S_1$

$l$  = length of slug =  $u \cdot t_e$  in horizontal

$\Delta x_1$  = dist. to receptor negative in this example with magnitude  $l - \Delta x_2$

$\therefore \Delta x_1 = -(l - \Delta x_2)$   
 $= \Delta x_2 - l$



$$c(\epsilon) = \frac{F \cdot g}{(2\pi)^{1/2} u' \sigma_y} \cdot g \cdot e^{-\frac{1}{2} \left(\frac{z}{\sigma_y}\right)^2 \left(\frac{u}{u'}\right)^2} \quad (2-14)$$

$$F = \frac{1}{2} \left\{ \operatorname{erf} \left( \frac{\Delta x_2}{2^{1/2} \sigma_{y_2}} \right) - \operatorname{erf} \left( \frac{\Delta x_1}{2^{1/2} \sigma_{y_1}} \right) \right\} \quad (2-15)$$

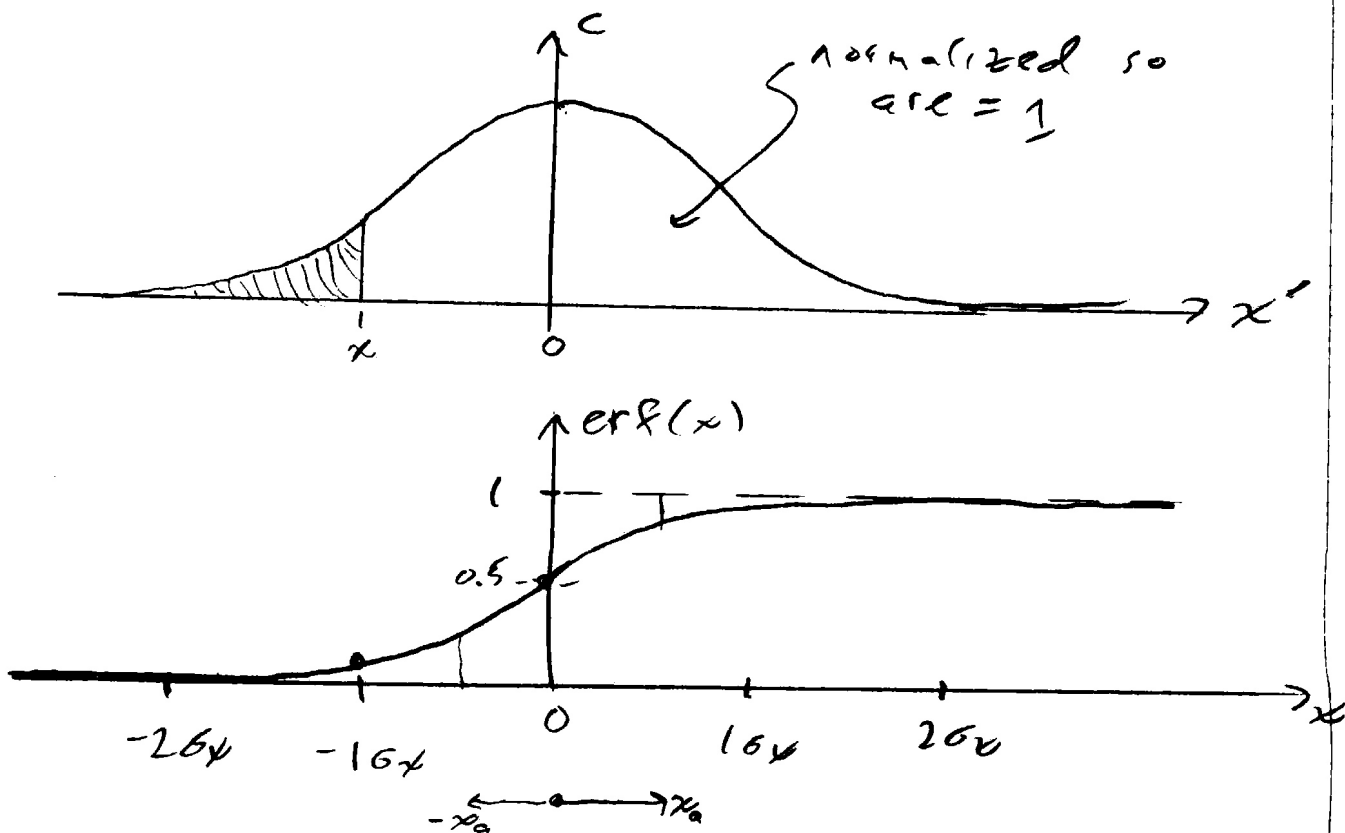
= "crossed to front"

$$g = \frac{2}{(2\pi)^{1/2} \sigma_z} \sum_{n=-\infty}^{\infty} e^{-\frac{1}{2} \left( \frac{H + 2nh}{\sigma_z} \right)^2}$$

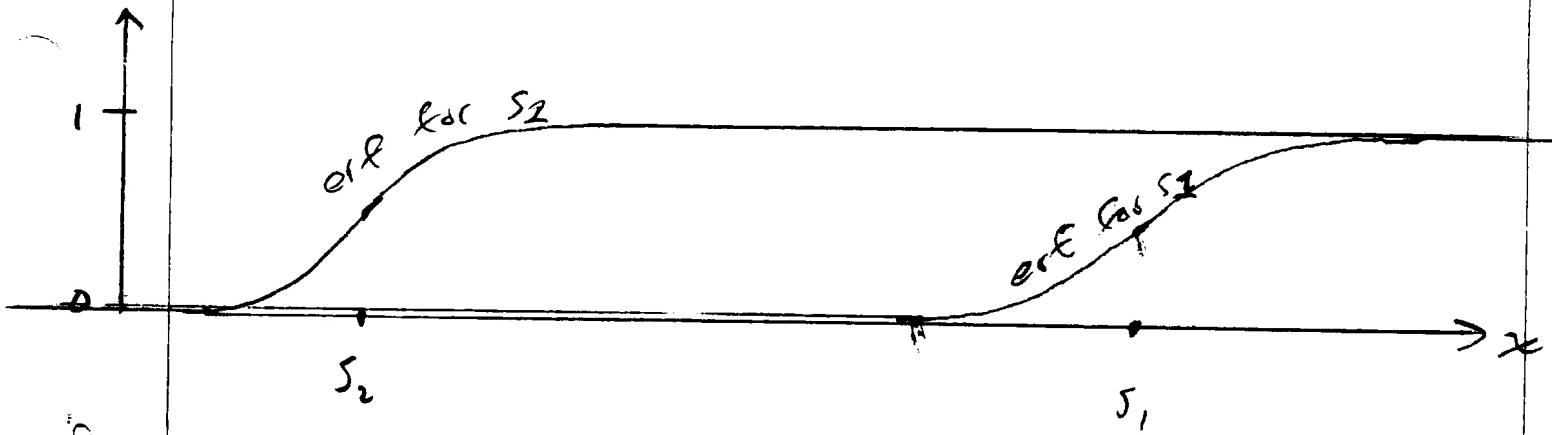
where  $u' \equiv (u^2 + \sigma_u^2)^{1/2}$

fudge to prevent divide-by-zero for calm winds  $u=0$ .

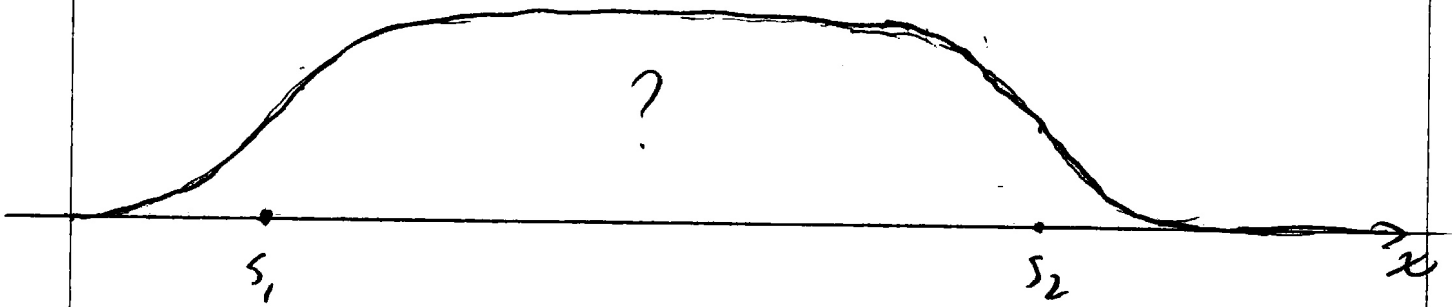
Recall  $\operatorname{erf}(x) = \int_{-\infty}^x G(x') dx'$



Note:  $\operatorname{erf}(-x_0) = 1 - \operatorname{erf}(x_0)$  by inspection



What do you get when you subtract erf for  $s_1$  from erf for  $s_2$ ?



Answer: you get a "slug".

What happens when  $u \rightarrow 0$

- Look at crosswind term: ?

→ 1

- Look at initial factor  $\frac{F \cdot q}{A \cdot \sigma}$  = ?

are the units reasonable?

- What happens to  $l$  = ? Answer:  $l \rightarrow 0$

- What happens to  $\Delta x_1$  = ? Answer:  $\Delta x_1 = \Delta x_2 = 0$

- What happens to the slug term  $F$ ?

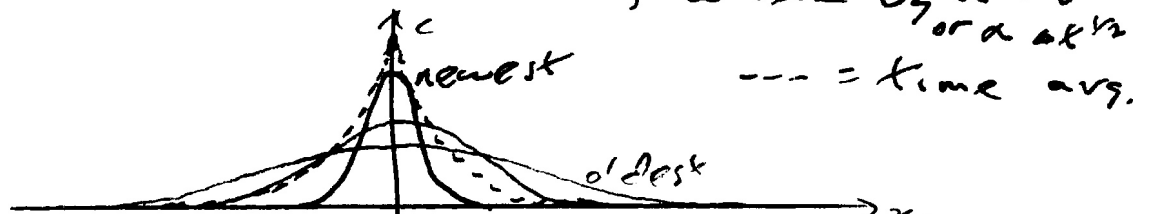
defour

- But the Tech Note (p2-8, last #) says

$$F \rightarrow -\text{erf}\left(\frac{\sigma x}{2\sqrt{\sigma_y}}\right)$$

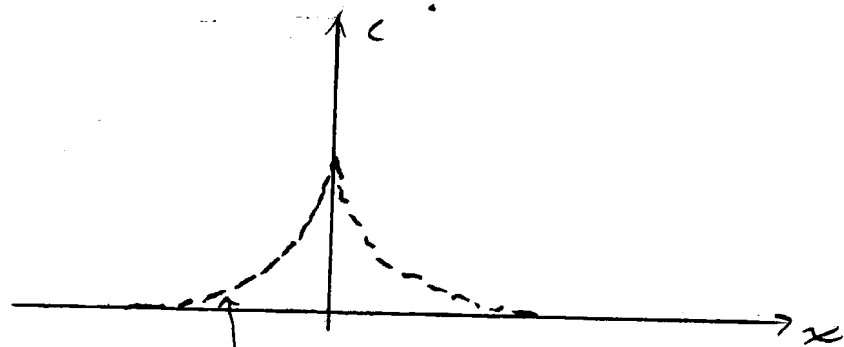
Why?

Answer: emissions are still happening over a finite time  $\Delta t$ , where  $\sigma_y \propto \Delta t$ .



continued next page

Answer continued:



$\bar{x}$  is the  $-x$  position of eff.

Is this true? Can check w/ HW

where  $\bar{\sigma}_y = \text{avg}(\sigma_y)$

- end of this lecture -

Recall from Taylor's' stat. theory

Near source (small times)

for  $t < t_L$

$$\sigma_y \approx \sigma_v(t)$$

Far from source (larger times)

for  $t > t_L$

$$\sigma_y \approx \sigma_v(2 \cdot t \cdot t_L)^{1/2}$$

where  $t_L = \text{Lagrangian time scale}$

$\approx 60 \text{ s.}$



But for air quality, need  $\bar{c}$  avg over time

p 2-9, eq 2-16 thru 2-20 is for the special case of -the newest slug where the  $S_2$  point is still at the emission source.

But can ignore this eq. -

Because the last sentence <sup>on p 2-9</sup> says that a more general solution is found by numerically integrating eq 2-14 over time.

You will do this in your HW (R, Matlab, Python)

Answers